

GAME-BASED HYBRID PARTICLE SWARM OPTIMIZATION OF JOB-SHOP PRODUCTION CONTROL

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Abstract

The traditional multi-objective particle swarm optimization (PSO) cannot effectively handle the production control problem involving multiple types of production lines or production objectives. Therefore, this paper designs a game-based hybrid PSO (GBHPSO) for job-shop production control. Firstly, a job-shop model was established with parts processing line, parts assembly line, and product assembly line, and the production control ideas were designed to combine real-time monitoring of events and operation sequence adjustment. Then, the production control objectives were determined for the three production lines. After that, the GBHPSO was applied to solve the job-shop production control problem, the product utility function was constructed, and the execution low was detailed for the solving algorithm. Experiments demonstrate the effectiveness of our algorithm. The research provides a reference for applying our algorithm in resource allocation of other production fields.

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Key Words: Game-Based Hybrid Particle Swarm Optimization (GBHPSO), Production Control, Product Utility

1. INTRODUCTION

With the advent of intelligent manufacturing, the various sensors of job-shop data acquisition and the Internet of things (IoT) for system interconnection have been increasingly applied to job-shop control [1-6]. The difficulty of job-shop control lies in the many uncertain disturbances in the processing environment and the complex changes of working conditions [7-10]. For the frequent disturbances, their degree of impact on job-shop production efficiency and control cost must be quantified. This is essential to the active job-shop scheduling and the early warning of disturbances, and meaningful for improving the rescheduling ability of the job-shop after being disturbed [11-14].

Yahouni et al. [15] constructed a multi-disturbance partition model for the discrete job-shop hierarchy tree; the model accurately defines the priorities of disturbance risk vectors, and differentiated between different types of disturbances. Guo [16] established a mathematical model of the time flow of job-shop operations under ideal and actual conditions, and realized the closed-loop control from discrete job-shop disturbance prediction to production based on the hybrid Bayesian decision tree algorithm. Nababan et al. [17] designed a multi-objective scheduling solving model to optimize the makespan and delivery delay of discrete job-shop, and completed real-time adjustment of some production operations of the job-shop, using the ADSM method. Jahan et al. [18] defined five basic job-shop elements, namely, product, output, technique, production assistance and production time, and created a lean job-shop production management system through systematic design planning (SLP).

Facing the diverse and fast changing market demand, the traditional methods for job-shop scheduling and product assembly cannot meet the requirements on logistics efficiency in the job-shop [19-22]. Bożejko et al. [23] fully considered the onsite job-shop management and intelligent logistics control, and provided the multi-objective optimization function and its constraints for minimizing the path length and distribution cost. The core of scientific job-shop production control is to support real-time interaction between information and managers, on the

premise of acquiring the various factors affecting product quality. However, it is often difficult to handle or prewarn the product quality problems on the site of job-shop production. To overcome the difficulty, Al Aqel et al. [24] proposed a job-shop product quality control system based on multiple mobile communication terminals, and explained the design flow of the hardware and software for subsystem interaction, quality prewarning, etc. Most assembly job-shops have problems like poor information interaction and difficulty in real-time monitoring. Through semantic data modelling, Wang et al. [25] unified the information interaction model between the objects of assembly job-shop production control, and realized the logical integration of the assembly system, such that the managers, machines, operators, and materials can operate in an integrated manner.

On job-shop production control, the traditional multi-objective particle swarm optimization (PSO) has relatively good convergence and diversity, when the production lines are independent or the production objectives are not very diversified. However, the traditional approach has great challenges if the working conditions are very complex. To effectively reduce the probability of the PSO falling into local optimum trap under complex working conditions, this paper puts forward a game-based hybrid PSO (GBHPSO) for job-shop production control. Section 2 creates a job-shop model containing parts processing line, parts assembly line, and product assembly line. Section 3 constructs the production control objectives for the three production lines. Section 4 solves the job-shop production control problem with GBHPSO, sets up product utility function and game model, and details the execution low of the solving algorithm. Experimental results show that our algorithm can improve the reliability and reasonability of job-shop production control to a certain extent.

2. JOB-SHOP STRUCTURE AND PRODUCTION CONTROL IDEAS

Fig. 1 shows the proposed job-shop model, which contains parts processing line, parts assembly line, and product assembly line. Before setting up the optimization objectives of the production control system for the job-shop model, the demands for parts should be smoothened, and the features of different production lines should be fully considered. If an uncertain delay event occurs in the job-shop, the information feedback and control of each production line should be rationalized through the production control that combines real-time event monitoring and operation sequence adjustment.

Then, the supply-demand details of each production line were supplemented. On this basis, the entity-relationship diagram of job-shop production control system was obtained (Fig. 2). The diagram presents an institutive picture of the relationship between warehouses, parts, components, and products, and provides the real-time data on the attributes of each entity.

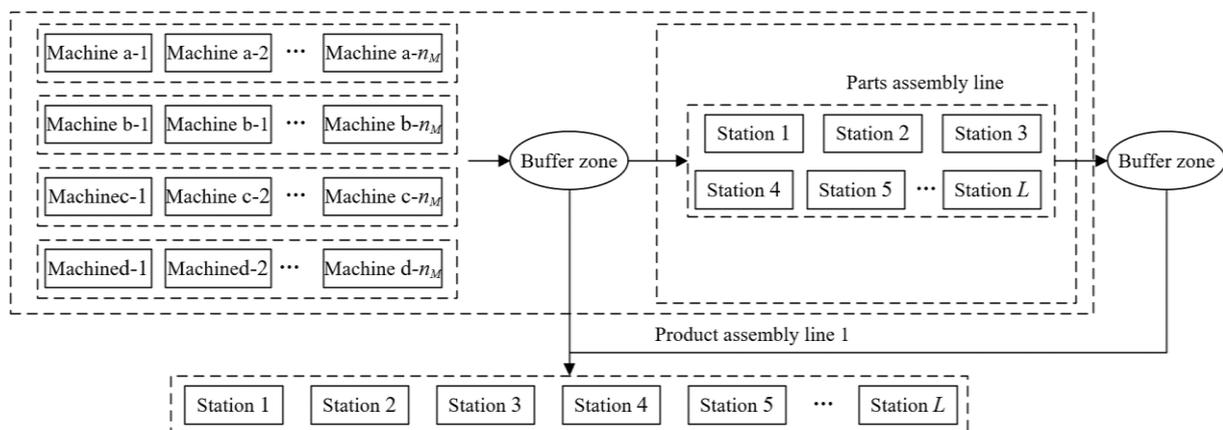


Figure 1: Structure of job-shop model.

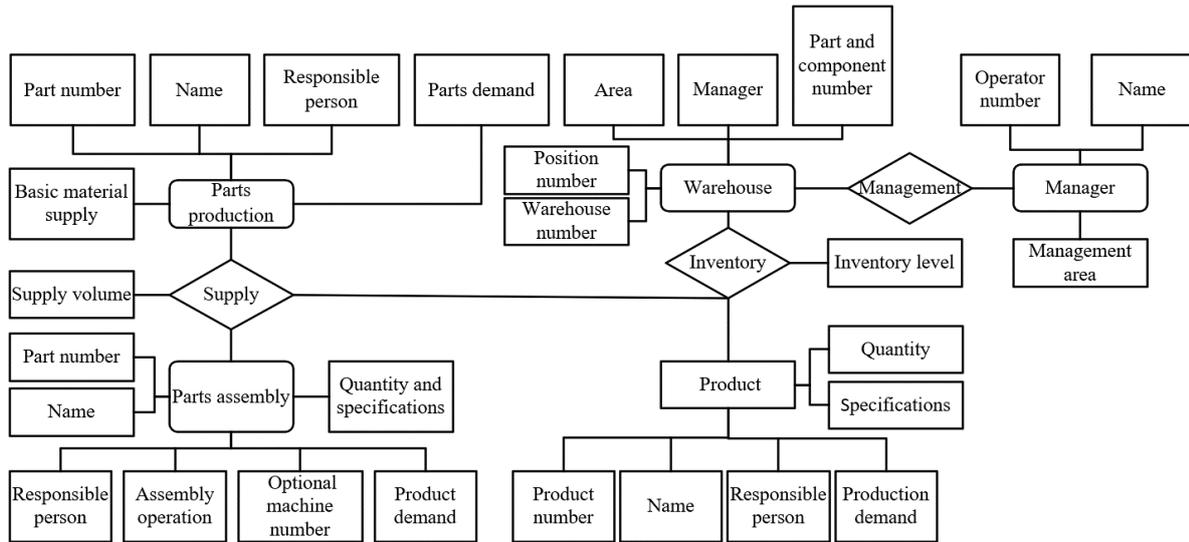


Figure 2: Entity-relationship diagram of job-shop production control system.

3. JOB-SHOP PRODUCTION MODELLING

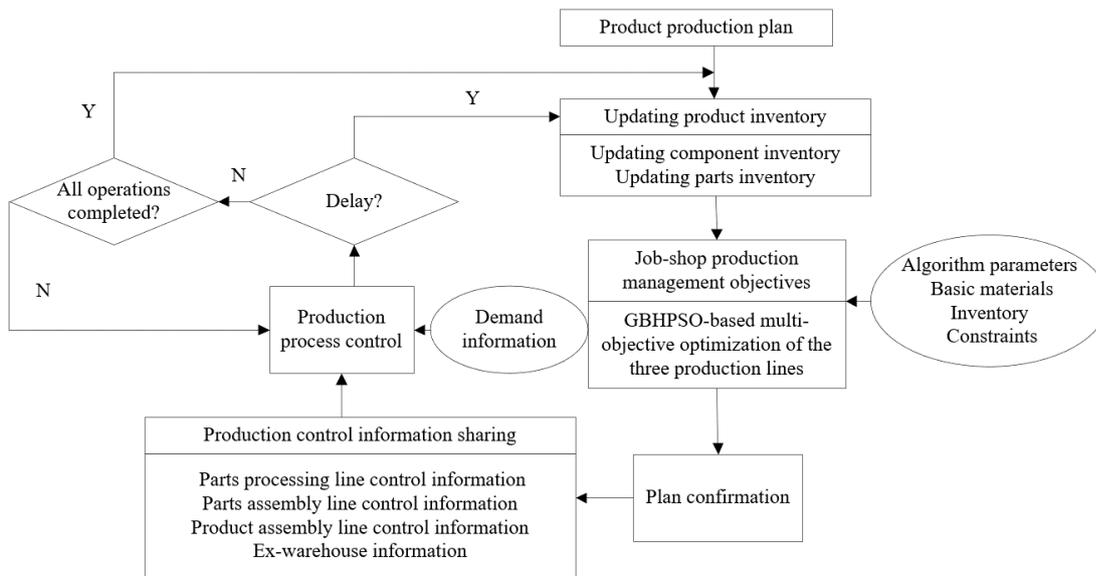


Figure 3: Flowchart of job-shop production control system.

3.1 Production control objectives of product assembly line

In the l^{th} production sequence, the number of i^{th} products is denoted as b_{il} ; the number of the j^{th} parts to be provided by the current station to assemble the b_{il} products is denoted as a_{ij} ; the total number of the j^{th} parts is denoted as m_j ; the inventory of the j^{th} parts in the buffer zone is denoted as HC_j ; the total number of positions and parts are denoted as L and J , respectively. Then, the objective function for smoothing the parts demand can be created as:

$$\min \sum_{j=1}^J \sum_{l=1}^L (a_{jl} - HC_j - l \times m_j / L)^2 \quad (1)$$

Eq. (1) tries to keep the actual demand for the part consistent with the mean demand. Let I be the number of products to be manufactured; w_{il} be an indicator about the station of the i^{th} product to be manufactured on the production line. Then, Eq. (1) should satisfy:

$$s.t. \quad w_{il} \in \{0,1\} \forall i \in I \quad l=1,2,\dots,L \quad (2)$$

Eq. (2) shows that w_{il} is a binary function. The value of that function is either zero or one. If the station corresponding to the l^{th} production sequence is only arranged one product:

$$\sum_{i \in I} w_{il} = 1 \quad \forall i = 1, 2, \dots, I \quad (3)$$

Let q_i and e_i be the target quantity and inventory of the i^{th} products, respectively. If the i^{th} products are arranged on the station corresponding to the l^{th} production sequence:

$$\sum_{l=1}^L w_{il} = q_i - e_i \quad \forall i \in I \quad (4)$$

The number of the i^{th} products can be expressed as:

$$b_{il} = \sum_{i=1}^L w_{il} \quad \forall l = 1, 2, \dots, L \quad (5)$$

Let s_{ij} be the number of j^{th} parts required for each product. Then,

$$b_{il} = \sum_{i=1}^k b_{il} s_{ij} \quad (6)$$

m_j can be calculated by:

$$m_j = \sum_{i=1}^L (q_i - e_i) s_{ij} \quad (7)$$

The completion time F_i and delivery date DP_i of the i^{th} product satisfy:

$$F_i \leq DP_i \quad (8)$$

3.2 Production control objectives of parts assembly line

Suppose J parts need to be assembled independently on the L stations of the parts assembly line. The J parts belong to the orders of Q products. Among them, the q^{th} product contains M_q parts: $H^{q_1}, H^{q_2}, \dots, H^{q_{M_q}}$, $\sum_{q=1}^M M_q = J$. Let $t_{lH_j^q}$ be the processing time of the j^{th} part H_j^q of the q^{th} product on the l^{th} station; TS_q be the processing time of M_q parts; OV_{jl}^q be the completion time of part H_j^q on station l . Then, the binary function $T(H_j^q)$ about whether a part is assembled on time can be established as:

$$T(H_j^q) = \begin{cases} 1 & OV_{jl}^q \leq TS_q \\ 0 & \text{others} \end{cases} \quad (9)$$

If $T(H_j^q) = 1$, the assemblage is on time; if $T(H_j^q) = 0$, the assemblage is delayed. The integrity coefficient Φ_q can be defined as:

$$\phi_q = \begin{cases} 1 & \sum_{j=1}^{M_q} T(H_j^q) = M_q \\ 0 & \sum_{j=1}^{M_q} T(H_j^q) < M_q \end{cases} \quad (10)$$

Let ω_q be the weight of the q^{th} product order. Then, we have the following model:

$$\max \sum_{q=1}^Q \omega_q \phi_q \quad (11)$$

Eq. (11) can be converted into:

$$\min \frac{1}{\sum_{q=1}^Q \omega_q \phi_q} \quad (12)$$

Let Δt_{H_j} be the waiting time for part H_j on the l^{th} station. Eq. (12) should satisfy:

$$s.t. \quad OV_{1,1}^1 = t_{1H_1^1} + \Delta_{1H_1} \quad (13)$$

The completion time of the first part in the parts assembly sequence on the first machine, and that of parts on the first station can be respectively obtained by:

$$OV_{1,1}^1 = OV_{1,(l-1)}^1 + t_{1H_1^1} + \Delta_{1H_1} \quad (14)$$

$$OV_{j,1}^q = OV_{h,1}^i + t_{1H_j^q} + \Delta_{1H_j^q} \quad (15)$$

Starting with the second sequence, the completion time of parts on the other stations can be obtained by:

$$OV_{j,l}^q = \max\{OV_{h,l}^i, OV_{j,(l-1)}^q\} + t_{1H_j^q} + \Delta_{1H_j^q} \quad (16)$$

Let W_{ctr} be the number of the c^{th} parts in the buffer zone at time τ ; W_{clH_j} be the total number of the c^{th} parts required for part H_j on the l^{th} station. Then, Δ_{1H_j} can be obtained by:

$$\Delta_{1H_j} = \begin{cases} \hat{\tau} - \tau & W_{ctr} < W_{clH_j} \\ 0 & W_{ctr} > W_{clH_j} \end{cases} \quad (17)$$

3.3 Production control objectives of parts processing line

The production control of parts processing line can be simplified as rationalizing the production sequence and operation interval of parts, with the aim to minimize the difference between completion time of parts and demand time. Let M_C and n_M be the number of parts and machines, respectively; OV_{cbl} , τ_{cbl} , and O_c be the completion time, processing time, and completion moment of the b^{th} operation of the c^{th} part on the l^{th} station, respectively; S_c be the start moment of the secondary operation after the completion of the c^{th} part. Then, an objective function can be established as:

$$\min \sum_{c=1}^{M_c} (OV_c - S_c) \quad (18)$$

Eq. (18) needs to satisfy the constraint on the processing time of the c^{th} part:

$$s.t. \quad OV_{ctr} - OV_{c(b-1)q} \geq \tau_{cbl} \quad (19)$$

Eq. (19) shows that the machine corresponding to the l^{th} station cannot start the b^{th} operation until completing the $(b-1)^{\text{th}}$ operation. The resource constraint on the l^{th} station can be given by:

$$OV_{qjl} - OV_{hel} \geq \tau_{qjl} \quad (20)$$

Eq. (20) shows that the l^{th} station cannot start processing another part until completing the processing of the current part. OV_{cbl} can be calculated by:

$$OV_{cbl} = \max(OV_{(c-1)hl}, OV_{c(b-1)q}) + \tau_{cbl} \quad (21)$$

4. GBHPSO-BASED PRODUCTION CONTROL STRATEGY

4.1 Algorithm design

Fig. 4 presents the game relationships between the independent production lines. It can be seen that the GBHPSO firstly quantifies the subjective factors of the management effect of each production line into computable form or analysable form based on the game theory, and then fuses the two kinds of factors into the PSO for each production line.

Let N_G be the number of particles in the swarm; e be the dimensionality of the search space. After r iterations, the position and velocity of the i^{th} particle can be described as $A_{ir} = (A_{ir}^1, A_{ir}^2, \dots, A_{ir}^e)$ and $v_{ir} = (v_{ir}^1, v_{ir}^2, \dots, v_{ir}^e)$, respectively, $i \in [r, N_G]$, $r \in [0, R_{max}]$. Suppose the global

optimal and local optimal are $G_b = (g_1, g_2, \dots, g_e)$ and $P_b = (p_i^1, p_i^2, \dots, p_i^e)$, respectively. The values of G_b and P_b can be derived from the fitness based on position vectors. Let θ be the dynamic inertial weight; σ_1 and σ_2 be the learning factors. Then, the particle velocity can be updated by:

$$v_{i,j}(\tau+1) = \theta v_{i,j}(\tau) + \sigma_1 \times \eta_1 \times [P_b(i,j) - A_{i,j}(\tau)] + \sigma_2 \times \eta_2 \times [G_b(j) - A_{i,j}(\tau)] \quad (22)$$

where, η_1 and η_2 are random numbers in $[0, 1]$. The particle position can be updated by:

$$A_{i,j}(\tau+1) = A_{i,j}(\tau) + v_{i,j}(\tau+1) \quad (23)$$

Let R and R_{max} be the current and maximum number of iterations, respectively. The value of θ can be obtained by:

$$\theta = \theta_{max} - r \frac{\theta_{max} - \theta_{min}}{R_{max}} \quad (24)$$

To prevent premature convergence caused by excessively fast velocity, the particle velocity is bounded by a maximum v_{max} and a minimum v_{min} . The positions A_i corresponding to the maximum and minimum velocities can be denoted as A_{max} and A_{min} , respectively.

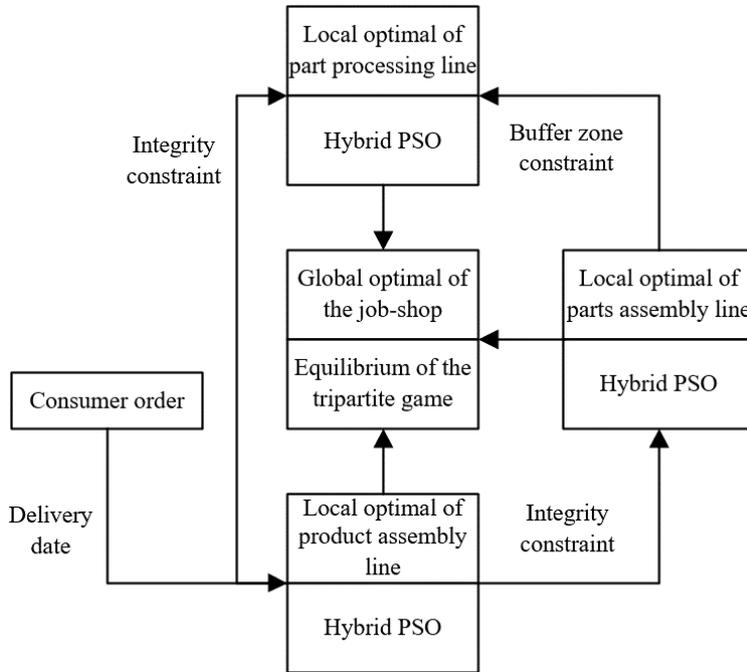


Figure 4: Game relationships between independent production lines.

4.2 Product utility function and game modelling

The cooperative relay game in the GBHPSO is equivalent to a Stackelberg game that includes a first-mover and a responder. As the first-mover, each station can set the unit price of the cooperation according to the total demand of all products to be manufactured. As the responder, each product can determine its ranking or share of processing and assembly operations according to the cooperation price.

Let $PR = \{1, 2, \dots, m_{pr}\}$ be the set of the products to be manufactured in the system; γ_i be the start moment of its operations applied by the production control strategy of the i^{th} product to the l^{th} station; $\gamma = \{\gamma_1, \dots, \gamma_{m_{pr}}\}$ be the set of the production control strategies of all products $\{\gamma_1, \dots, \gamma_{m_{pr}}\}$. Then, the pricing strategy of the l^{th} station can be defined as:

$$BU(l) = s \left(\sum_{i=1}^{m_{pr}} \gamma_i \right)^\zeta \quad (25)$$

If the total processing time of all products exceeds the working time limit of the station node, the station will reject the product requiring the shortest processing time, in order to maximize its utility. In addition, the station offers all products the same price.

In the GBHPSO, every network node hopes to obtain more processing time SH at a small cost Ψ . During the cooperation, the nodes seek a compromise by the energy efficiency function $v = SH/\Psi$. When the product demand at the start moment is γ , the utility function can be expressed as:

$$O_i = (SH_{c_i, e_i}(\Psi_i, \gamma - \gamma_i) + SH_{c_i, e_i}^*(\Psi_i, \gamma_i)) / \Psi_i - BU \cdot \gamma_i \quad (26)$$

Let K and D be the delay and actual processing time, respectively. Then, $SH_{c_i, e_i}(\Psi_i, \gamma - \gamma_i) = (\gamma - \gamma_i)g(\beta_{bi, ei})K/D$ is the time consumed by the i^{th} product on a randomly selected station during the period $\gamma - \gamma_i$. $SH_{c_i, e_i}^*(\Psi_i, \gamma_i) = \gamma_i g(\beta_{bi, ei}^*)K/D$ is the time consumed by the i^{th} product and the l^{th} station, which jointly occupies the start moment γ_i . The i^{th} product needs to pay $BU \gamma_i$ for the occupation.

To find the equilibrium solution to the cooperative game between all products and stations, it is necessary to determine the optimal strategy of the game parties. Combining Eqs. (25) and (26):

$$O_i = \frac{K\gamma}{D\Psi_i} g(\beta_{c_i, e_i}) + \frac{K\gamma_i}{D\Psi_i} g(\beta_{c_i, e_i}^*) - \gamma_i \left(s \left(\sum_{j=1}^{m_{pr}} \gamma_j \right)^\zeta \right) \quad (27)$$

where, $g(\beta_{c_i, e_i}^*, \beta_{c_i, e_i}) = g(\beta_{c_i, e_i}^*) - g(\beta_{c_i, e_i})$ is the time gain of the completion time through the cooperative production of the i^{th} product over that of a randomly selected station. Eq. (27) shows that the utility of each product is affected by the production control strategy of every other product in the network. Let $\gamma_i' = \{\gamma_j'\}_{j=1, j \neq i}^{m_{pr}}$ be the set of optimal production control strategies of all the products other than the i^{th} product. Then, the optimal strategy of the i^{th} product can be expressed as:

$$\gamma_i' = \max \left(0, \arg \max_{\gamma_i} O_i(\gamma_i, \gamma_i') \right) \quad (28)$$

The above equilibrium strategy is not optimal for the global utility of all the products to be manufactured in the job-shop. To improve the utility of all products, the Pareto optimal solution can be constructed as:

$$O_i^\mu = \frac{K\gamma}{D\Psi_i} g(\beta_{c_i, e_i}) + \frac{K\mu\gamma_i'}{D\Psi_i} \Delta g(\beta_{c_i, e_i}^*, \beta_{c_i, e_i}) - \mu\gamma_i' \left(s \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^\zeta \right) \quad (29)$$

Suppose under the equilibrium strategy $\{\gamma_i'\}_{i=1}^{m_{pr}}$, all products change its start moment of its operations with parameter $\mu (\mu > 0)$. Then, the new set of production control demands can be described as $\{\mu\gamma_i'\}_{i=1}^{m_{pr}}$. Under the new strategy, the utility function of the i^{th} product can be given by:

$$\frac{\partial O_i^\mu}{\partial \mu} = \frac{K\gamma_i'}{D\Psi_i} \Delta g(\beta_{c_i, e_i}^*, \beta_{c_i, e_i}) - s\gamma_i' (1 + \zeta) \mu^\zeta \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^\zeta \quad (30)$$

According to Eq. (28), the equilibrium conditions can be defined as:

$$\frac{K}{D\Psi_i} \Delta g(\beta_{c_i, e_i}^*, \beta_{c_i, e_i}) = s \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^\zeta + \zeta \gamma_i' \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^{\zeta-1} \quad (31)$$

Combining Eqs. (30) and (31):

$$\frac{\partial O_i^\mu}{\partial \mu} = s\gamma_i' \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^\zeta (1 - \mu^\zeta) + s\zeta \gamma_i' \left(\sum_{j=1}^{m_{pr}} \gamma_j' \right)^{\zeta-1} \left(\gamma_i' - \mu^\zeta \sum_{j=1}^{m_{pr}} \gamma_j' \right) \quad (32)$$

Whether the equilibrium strategy is Pareto optimal can be judged by:

$$\frac{\partial O_i^\mu}{\partial \mu} \Big|_{\mu=1} = s\zeta \gamma'_i \left(\sum_{j=1}^{m_{pr}} \gamma'_j \right)^{\zeta-1} \left(\sum_{j=1, j \neq i}^{m_{pr}} \gamma'_j \right) \quad (33)$$

Since γ'_i , s , and ζ are greater than zero, $\frac{\partial^2 O_i^\mu}{\partial \mu^2} \Big|_{\mu=1}$ must be negative. This means the original equilibrium strategy is not optimal.

4.3 Algorithm flow

The flow of the job-shop production control problem by the GBHPSO is detailed in Fig. 5.

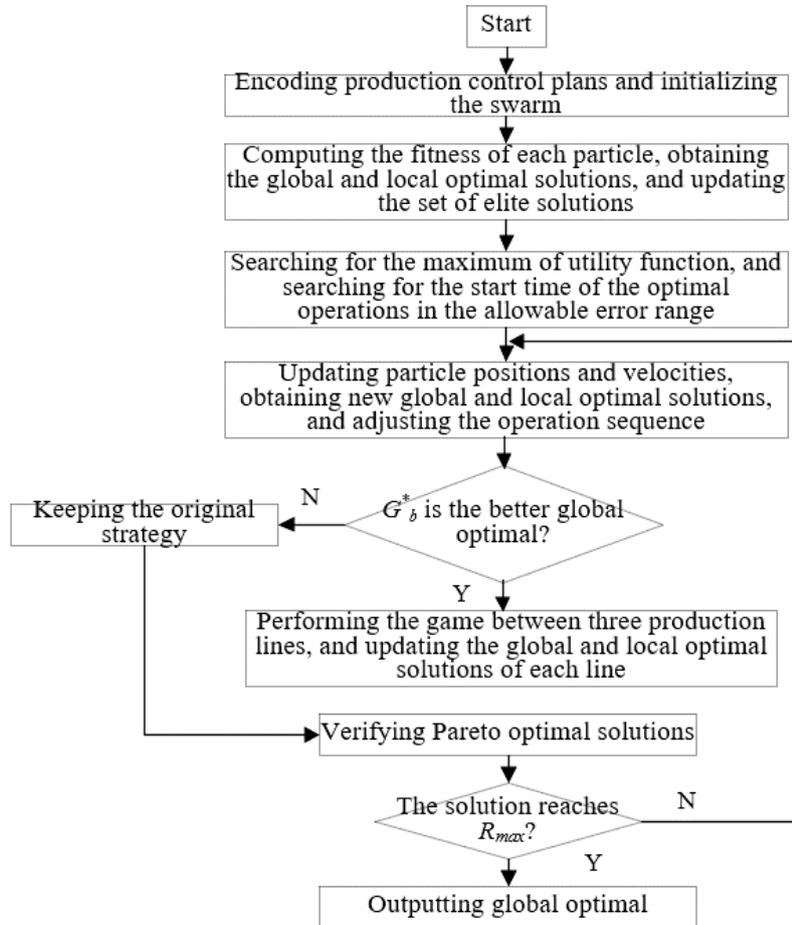


Figure 5: Flowchart of our algorithm.

5. EXPERIMENTS AND RESULTS ANALYSIS

To verify the effectiveness of our algorithm on production scheduling of job-shops involving multiple production lines, the production control strategy was studied for an industrial job-shop of an industrial manufacturer producing various kinds of products. The job-shop contains six machines. Table I presents the operation time of each operation in product assembly. Table II presents the operation time of each operation in parts assembly.

Figs. 6 and 7 are the Gantt charts of product assembly and parts assembly, respectively. The x- and y-axes represent machine number and production time, respectively; nm stands for the m^{th} operation of the n^{th} product or part. It can be seen that the assembly operations on the two lines are arranged uniformly, indicating that our algorithm can effectively improve the reliability and reasonability of job-shop production control.

Table I: Operation time of each operation in product assembly.

Operation number	A	B	C	D	E	F
1	24	13	25	33	21	22
2	21	20	27	26	24	25
3	43	22	56	44	21	43
4	25	59	22	28	56	21
5	41	38	19	12	26	16

Table II: Operation time of each operation in parts assembly.

Machine number	<i>a</i>		<i>b</i>		<i>c</i>	
	Operation	Time	Operation	Time	Operation	Time
1	1	11	1	13	1	17
2	2	13	2	16	2	14
3	3	13	3	15	3	13
4					4	11
5						
6	4	14	4	12		
Machine number	<i>d</i>		<i>e</i>		<i>f</i>	
	Operation	Time	Operation	Time	Operation	Time
1			1	17	1	15
2	1	16				
3	2	15			2	16
4			2	16		
5	3	17	3	13	3	12
6	4	11	4	15	4	11

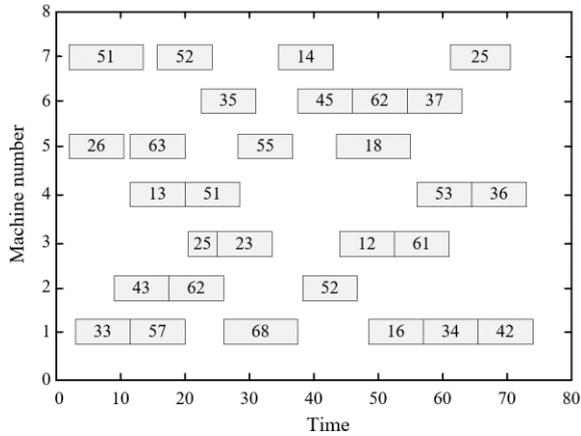


Figure 6: Gantt chart of product assembly.

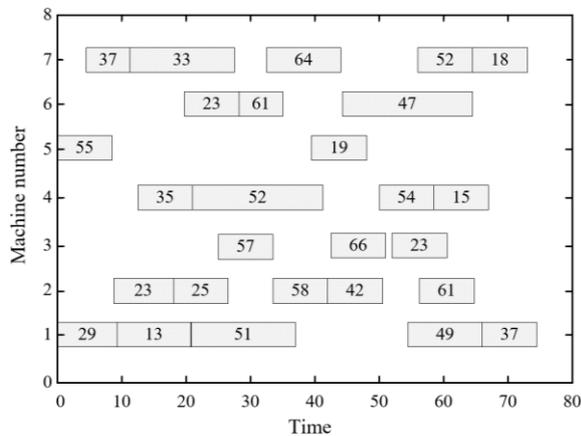


Figure 7: Gantt chart of parts assembly.

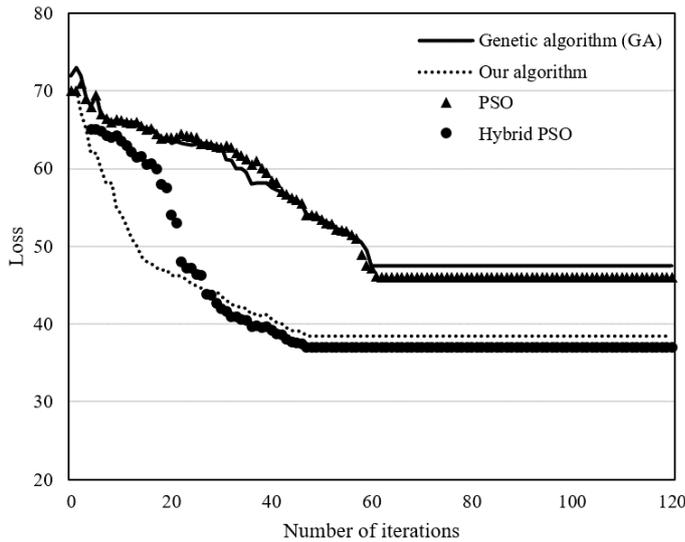


Figure 8: Iterative losses of different algorithms.

Based on the previously collected real-time data on each entity, the performance of our algorithm was further verified through comparative analysis. The swarm size was initialized as 500; the maximum number of iterations was set to 150; the mutation rate was defined as 6%. Then, the iterative process of our GBHPSO was compared with that of other algorithms on MATLAB. Obviously, our algorithm converged faster than the other algorithms. Therefore, the introduction of position vector effectively improves the ranking of operations.

Table III compares the processing time computed by different algorithms. It can be seen that our algorithm is superior to the traditional hybrid PSO in the processing time on each production line, and ends up with a smaller solving error.

Table III: Processing time computed by different algorithms.

Algorithm	Production line	Processing time	Error
Our algorithm	Product assembly	352	0.02
	Parts assembly	241	0.01
	Parts processing	157	0.01
Traditional hybrid PSO	Product assembly	387	-11.9
	Parts assembly	253	6.1
	Parts processing	175	7.9

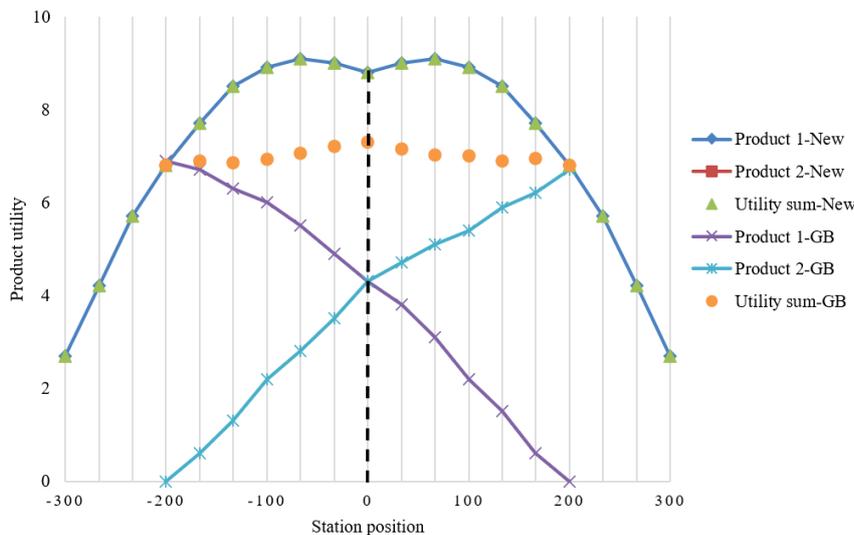


Figure 9: Global optimal product utility vs. Pareto optimal product utility.

Fig. 9 compares the product utilities obtained under the global optimal and Pareto optimal approaches. When two products apply for assembly to the same machine (i.e., the product assembly demands occur at the same time), the product utility of global optimal strategy was slightly lower than that of Pareto optimal strategy, owing to the competition between products. This is because, under Pareto optimal solution, the products and stations maximize their utilities through cooperation. By contrast, the hybrid PSO prioritizes the objectives of independent production lines. This non-cooperative equilibrium strategy could not maximize the overall utility of the job-shop.

6. CONCLUSIONS

This paper applies the GBHPSO to explore the production control strategy for job-shop. Specifically, a job-shop model involving multiple different production lines was established, and the production control ideas were presented, which combine real-time monitoring of delay events and operation sequence adjustment. Then, the production control objectives were defined for parts processing line, parts assembly line, and product assembly line. Next, the workflow of solving job-shop production control problem with GBHPSO was detailed. Through experiments, the Gantt charts of product assembly and parts assembly were obtained, and compared to verify the effectiveness of GBHPSO. Our algorithm was also compared with other methods in iterative losses and processing times. The comparison reveals the superiority of our algorithm in convergence speed and processing time. Finally, the global optimal strategy was contrasted with Pareto optimal strategy in terms of product utility. The results confirm that our algorithm has an advantage in maximizing the overall utility of the job-shop.

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